# Phase diagram of softly repulsive systems: The Gaussian and inverse-power-law potentials

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(Received 29 July 2005; accepted 22 August 2005; published online 11 October 2005)

We redraw, using state-of-the-art methods for free-energy calculations, the phase diagrams of two reference models for the liquid state: the Gaussian and inverse-power-law repulsive potentials. Notwithstanding the different behaviors of the two potentials for vanishing interparticle distances, their thermodynamic properties are similar in a range of densities and temperatures, being ruled by the competition between the body-centered-cubic (bcc) and face-centered-cubic (fcc) crystalline structures and the fluid phase. We confirm the existence of a reentrant bcc phase in the phase diagram of the Gaussian-core model, just above the triple point. We also trace the bcc-fcc coexistence line of the inverse-power-law model as a function of the power exponent n and relate the common features in the phase diagrams of such systems to the softness degree of the interaction. © 2005 American Institute of Physics. [DOI: 10.1063/1.2064639]

#### I. INTRODUCTION

A recurrent issue in statistical physics is the prediction of the phase behavior of a macroscopic system from the knowledge of the force law which rules the interaction between the constituent particles. Over the last decades, significant progress has been made in fulfilling this task, at least for simple model systems of classical point particles interacting through a spherically symmetric pair potential v(r). In particular, continuous advancements in both computer simulation methods and density-functional theory have revealed a few general features of the freezing transition, a phase change that is prominently driven by the repulsive component of the interatomic potential. For assigned thermodynamic conditions, the softness of the repulsion substantially determines the nature of the incoming solid phase. In fact, a rigid potential favors a more compact phase, such as the face-centered-cubic (fcc) or the hexagonal-close-packed (hcp) crystalline structure, as opposed to, say, the bodycentered-cubic (bcc) one. This is largely true even for more complex substances such as those that are generically classified as soft materials, such as colloidal suspensions for which the effective pair interactions can be accurately tailored through a fine experimental control of suspended particle and solvent properties.<sup>1,2</sup> A scholastic example is offered by the entropy-driven repulsion between (the centers of mass of) self-avoiding polymer coils dispersed in a good solvent.<sup>2–4</sup> In this specific case, the repulsion happens to be finite even if

$$v_G(r) = \epsilon \exp\left(-\frac{r^2}{\sigma^2}\right). \tag{1.1}$$

In Eq. (1.1) the length  $\sigma$  is of the order of the gyration radius of the polymer while the (positive) energy  $\epsilon$  is of the order of  $k_BT$ , where T is the temperature and  $k_B$  is the Boltzmann constant. However, it is also useful to study this potential without assuming an explicit dependence of  $\epsilon$  and  $\sigma$  upon the temperature. The model is then referred to as the Gaussian-core model (GCM). Other examples of softly repulsive fluids are provided by dilute solutions of colloidal particles, sterically stabilized against coagulation through a polymer coating. In this case, the strength and range of the effective repulsion between a pair of particles are determined by the thickness of the layer of grafted polymer chains and can be modeled with an inverse-power-law (IPL) potential,

$$\nu_n(r) = \epsilon \left(\frac{\sigma}{r}\right)^n,\tag{1.2}$$

upon choosing a suitable power exponent n. In the past, this potential has been also used for a simplified description of the thermal behavior of various simple metals under extreme thermodynamic conditions.<sup>6,7</sup>

With the advent of numerically accurate techniques for the calculation of the Helmholtz free energy of a solid, computer simulation has become a valuable tool for the determination of fluid-solid and solid-solid coexistence lines. Most notably, the Frenkel-Ladd (FL) method can be used in conjunction with conventional thermodynamic integration tech-

<sup>&</sup>quot;particles" fully overlap and can be modeled with a Gaussian-shaped potential,

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niques to calculate the "exact" phase diagram of the system, the only source of error being ultimately associated with the quality of the statistical sampling of the (finite) system.<sup>8–10</sup> Full-fledged computer studies have been carried out for the repulsive Yukawa potential, 11,12 typically used to model solutions of charged colloids with counterions, <sup>13,14</sup> and for the logarithmic-plus-Yukawa potential modeling star-polymer interactions. 15-17 In this paper, we present accurate results for the phase diagrams of the Gaussian-core model and of the inverse-power-law potential, with the aim of providing a comparable benchmark for such two potentials. A preliminary report on the present findings for the GCM has been already given in Ref. 18. The main results of this study are (i) the discovery of a reentrant bcc phase in the phase diagram of the GCM, (ii) an accurate determination of the bccfcc coexistence point of the IPL potential as a function of the softness parameter 1/n, and (iii) the formulation of an argument that accounts for the similarity of the low-density/lowtemperature behavior exhibited by the two models.

## **II. MODELS AND METHOD**

### A. The Gaussian-core model

As is well known, the freezing transition of a manyparticle system is ultimately promoted by the Pauli repulsion between inner-shell electrons, causing the effective interatomic potential to diverge at short distances. It is probably less known that the existence of a thermodynamically stable solid does not require a singular repulsion for vanishing interatomic separations. In fact, even a finite square-barrier potential (penetrable spheres) can support a stable solid phase at all temperatures. 19,20 In this respect, the Gaussian potential is a more realistic form of bounded repulsion. The GCM was originally introduced by Stillinger.<sup>5</sup> Two distinctive features of the phase diagram of the GCM, that are absent in other bounded-interaction models, are the existence of a maximum melting temperature  $T_{\text{max}}$ , and, correspondingly, of a reentrant melting transition into a denser fluid phase for  $T < T_{\text{max}}$ . In his original paper on the GCM, Stillinger noted that, in the limit of vanishing temperature and density, the Gaussian particles behave as hard spheres with a increasingly larger diameter. In the same limit, the fluid freezes into a fcc structure whose number density  $\rho$  vanishes with the temperature T (from now on, temperature, pressure, and density will be given in reduced units, i.e.,  $T^* = k_B T / \epsilon$ ,  $P^*$  $=P\sigma^3/\epsilon$ , and  $\rho^*=\rho\sigma^3$ ). The calculation of the total energy of different cubic structures shows that the fcc structure is favored, at zero temperature, for reduced densities lower than  $\pi^{-3/2} \simeq 0.1796$ . Beyond this threshold, a bcc solid takes over. However, upon compression, any regular arrangement of particles is eventually doomed to collapse for any T>0 (reentrant melting). 21,24 An extended study of the GCM phase diagram was carried out by Lang et al. who employed an integral-equation theory for the fluid phase and a harmonic approximation for the crystalline phases.<sup>23</sup> In this combined approximation, these authors estimated a maximum melting temperature  $T^*_{\rm max}$ =0.0102 at which the coexisting fluid and bcc phases have a reduced density  $\rho^*_{\rm max}$ =0.2292. They also found that the fcc-bcc coexistence lines run linearly from the

points  $\rho_{\text{fcc}}^* = 0.17941$  and  $\rho_{\text{bcc}}^* = 0.17977$  at  $T^* = 0$  to the points  $\rho_{\text{fcc}}^* = 0.16631$  and  $\rho_{\text{bcc}}^* = 0.16667$  at the triple-point temperature  $T_{\text{tr}}^* = 0.008753$ .

## B. The inverse-power-law fluid

The IPL potential has been the subject of many studies.<sup>25-27</sup> This potential provides a continuous path from hard spheres  $(n \rightarrow \infty)$  to the one-component plasma (n=1). Actually, a neutralizing background is needed for  $n \le 3$  to balance the nonintegrable long-ranged repulsion.<sup>28,29</sup> The thermodynamic properties of the model can be expressed in terms of just one quantity,  $\gamma = \rho^* T^{*-3/n}$ , as a result of the scaling properties of the excess Helmholtz free energy. Hence, for any given n, it is sufficient to trace the thermal behavior of the IPL fluid as a function of  $\rho^*$  along the isotherm  $T^* = 1$ . For large values of n, the bcc phase is found to be unstable with respect to shear modes. As a result, the fluid freezes into a fcc solid. As n decreases, the potential becomes increasingly softer and longer ranged until, for  $n \approx 8$ , the bcc phase becomes mechanically stable. For smaller values of n and for densities close to freezing, the entropy of the bcc solid turns out to be greater than that of the fcc phase since the former structure can actually sustain a larger number of soft shear modes. However, the fcc phase is favored at high densities and low temperatures because of its smaller energy. Hence, upon reducing  $\gamma$ , a fcc-bcc transition may actually anticipate the melting of the solid for intermediate values of n. Agrawal and Kofke located the triple point in the range of  $0.11 \lesssim 1/n \lesssim 0.17$ , further claiming that a more realistic estimate of the lower bound, based on the mechanic stability range of the bcc phase, was 0.1305.<sup>27</sup> However, they did not provide a direct and systematic estimate of the location of the fcc-bcc transition as a function of the power exponent n.

# C. Details of the Monte Carlo simulation

We performed Monte Carlo (MC) simulations of the GCM and of the IPL model in the canonical ensemble, implementing the standard Metropolis algorithm with periodic boundary conditions and with the nearest-image convention. The number of particles N was chosen so as to fit a cubic box of volume V with an integer number of cells: N  $=4m^3$  for the fcc solid and  $N=2m^3$  for the bcc solid, m being the number of cells along any spatial direction. The nearestneighbor distance a is  $(\sqrt{2}/2)(L/m)$  for a fcc lattice and  $(\sqrt{3}/2)(L/m)$  for a bcc lattice, where  $L=(N/\rho)^{1/3}$ . Our typical samples consisted of 1372 particles in the fluid phase and in the solid fcc phase, and of 1458 particles in the bcc phase. We emphasize that, unless one resorts to some extrapolation to infinite size (a computationally demanding task), one should compare the statistical properties of samples with similar sizes, in particular, if one wants to investigate the relative thermodynamic stability of different phases at given temperature and pressure. Occasionally, we considered smaller as well as larger sizes to check whether our results could be possibly affected by a significant size dependence

(and they were actually not). We also carried out a number of simulations of a hcp solid hosting  $10 \times 12 \times 12 = 1440$  particles.

In order to locate the freezing point at a given temperature, we generated distinct chains of simulations, starting from the very dilute fluid on one side and from the dense solid on the other side. As a rule, the last MC configuration produced for a given value of  $\rho$  was used, after a suitable rescaling of particle coordinates, as the starting point for the next run at a slightly higher or lower density. We monitored the difference in energy and pressure between the various phases until we observed a sudden change of both quantities, so as to avoid averaging over heterogeneous thermodynamic states. Usually, the solid can be overheated for a few more steps beyond the melting point. The undercooling of the fluid is notoriously much easier. For any  $\rho$  and T, the equilibration of each sample typically took a few thousand MC sweeps, a sweep consisting of one attempt to change sequentially the position of all the particles. The maximum random displacement of a particle in a trial MC move was adjusted once a sweep during the run so as to keep the acceptance ratio as close to 50% as possible, only small excursions around this value being allowed. Thermodynamic averages were computed over trajectories  $3 \times 10^4$  sweeps long. The pressure was computed through the virial formula:

$$P = \rho k_B T + \frac{1}{3V} \left\langle -\sum_{i < j} r_{ij} v'(r_{ij}) \right\rangle, \tag{2.1}$$

where  $r_{ij}$  is the distance between particles i and j and  $\langle \cdots \rangle$  denotes the canonical average. For the IPL fluid, the excess pressure is proportional to the excess energy  $u_{\rm ex}$  since  $-rv_n'(r)=nv_n(r)$ . To avoid counting pair interactions twice, the potential was truncated at a cutoff distance  $r_c$ , which was taken to be just slightly smaller than L/2. Correspondingly, long-range corrections to the energy and pressure were calculated upon assuming the radial distribution function (RDF) g(r) to be unity for  $r > r_c$ . The histogram of g(r) was constructed with a spatial resolution  $\Delta r = \sigma/50$  and was updated every 10 MC sweeps. The RDF was never found to differ significantly from unity—in any phase—at the maximum distance L/2, at least for the largest sample sizes.

The numerical estimate of statistical errors is a critical issue whenever different candidate solid structures so closely compete for thermodynamic stability. To this aim, we divided the MC trajectory into ten blocks and estimated the error bars to be twice as large as the standard deviation of the block averages, under the implicit assumption that the decorrelation time of any relevant variable was less than the size of a block. Typically, the relative errors affecting the energy and pressure of the fluid were found to be a few hundredths percent at the most (for a solid, they were even smaller). We computed the difference between the excess free energies of any two equilibrium states (say, 1 and 2) belonging to the same phase with the standard thermodynamic integration technique, i.e., via the combined use of the formulas:

$$\frac{f_{\rm ex}(\rho, T_2)}{T_2} = \frac{f_{\rm ex}(\rho, T_1)}{T_1} - \int_{T_1}^{T_2} dT \frac{u_{\rm ex}(\rho, T)}{T^2},$$
 (2.2)

and

$$\beta f_{\rm ex}(\rho_2, T) = \beta f_{\rm ex}(\rho_1, T) + \int_{\rho_1}^{\rho_2} d\rho \frac{1}{\rho} \left[ \frac{\beta P(\rho, T)}{\rho} - 1 \right].$$
(2.3)

In the above equations,  $f_{\rm ex}$  is the excess Helmholtz free energy per particle and  $\beta = (k_B T)^{-1}$ . The integrals in Eqs. (2.2) and (2.3) were performed numerically with Simpson's rule over a cubic-spline approximant of the simulation data. The excess values of the chemical potential and of the entropy per particle follow from

$$\beta \mu_{\text{ex}} = \beta f_{\text{ex}} + \frac{\beta P}{\rho} - 1$$
 and  $\frac{s_{\text{ex}}}{k_{\text{B}}} = \beta (u_{\text{ex}} - f_{\text{ex}}).$  (2.4)

Equations (2.2) and (2.3) are useless if an independent estimate of the free energy is not available for some selected reference state of each phase. The free energy of a solid can be obtained with the FL method, that is reviewed in the next paragraph. As for the fluid, a reference state can be any equilibrium state characterized by a very small density (a nearly ideal gas), since then the excess chemical potential  $\mu_{\rm ex}$  can be accurately estimated through Widom's particle-insertion method.  $^{10,30}$ 

$$\mu_{\rm ex} = -k_B T \ln \langle \exp(-\beta E_{\rm ins}) \rangle, \tag{2.5}$$

where  $E_{\rm ins}$  includes all the interactions between a randomly inserted test particle and the particles of the fluid. Typically, the average in Eq. (2.5) was computed over equilibrium runs  $6 \times 10^4$  sweeps long, an insertion being attempted at the completion of each sweep.

The chemical potential is the quantity that decides which phase is stable for given values of T and P. Hence, it is necessary to inspect the error affecting this quantity with care. Let us consider, for instance, the chemical potential of a solid whose density is  $\rho_2$  in a state that is connected, along an isothermal path, to another (reference) state with density  $\rho_1$ . Let  $\delta f_1$  be the numerical precision of the FL calculation of the free energy of the reference solid. For each N-V-T simulation carried out along the isothermal path, one can estimate the error affecting the compressibility factor  $\beta P/\rho$ , whence its mean error  $\delta z$  along the path. Hence, according to Eqs. (2.3) and (2.4), the error affecting  $\mu$  is approximately given by  $\delta f_1 + k_B T \delta z (1 + \ln(\rho_2/\rho_1))$ .

# D. The Frenkel-Ladd calculation of the solid free energies

The method proposed by Frenkel and Ladd to calculate the free energy of a solid relies on a different kind of thermodynamic integration. The idea is to connect continuously the state of a solid (say, system 1 with potential energy  $V_1$ ), to the state of another solid (say, system 0 with potential energy  $V_0$ ) whose free energy is known. Upon assuming the reference solid to be an Einstein solid with spring constant c, a hybrid system is sampled with potential

 $V_{\lambda} = V_0 + \lambda(V_1 - V_0)$  ( $0 \le \lambda \le 1$ ), for given  $\rho$  and T. The Helmholtz free energy of system 1 is then obtained through Kirkwood's formula:

$$F_1 - F_0 = \int_0^1 \mathrm{d}\lambda \langle V_1 - V_0 \rangle_\lambda. \tag{2.6}$$

The free energy of the Einstein solid and the mean-square separation of an Einstein particle from its reference lattice site are

$$\beta F_0 = -\frac{3N}{2} \ln \left( \frac{2\pi}{\Lambda^2 \beta c} \right), \tag{2.7}$$

$$\Delta R_0^2 = \frac{3}{\beta c},\tag{2.8}$$

where  $\Lambda$  is the thermal wavelength. A nontrivial problem with this choice of  $V_0$ , already pointed out in the original paper, so the following: The Einstein particles can only perform limited excursions about their reference lattice positions, which implies a finite value of  $\Delta R^2$ ; however, there is no means to constrain particles interacting with the potential  $V_1$  to move within the neighborhood of their initial positions, even in the solid phase. In other words, at variance with  $V_0$ ,  $V_1$  is a translationally invariant potential, which implies that the integrand in Eq. (2.6) diverges for  $\lambda = 1$ . This problem can be overcome by performing MC simulations of  $V_{\lambda}$  under the constraint of a fixed center of mass. Only afterwards, the proper corrections are taken into account. We just quote the final result:

$$\beta f_{\rm ex}(N) = \frac{\beta V_1^{(0)}}{N} - \ln(\rho(\beta c)^{-3/2}) - \frac{3}{2} \ln(2\pi) + 1 - \frac{2 \ln N}{N} + \frac{\ln(2\pi)}{N} + \frac{\ln(\rho(\beta c)^{-3/2})}{N} + \frac{\beta}{N} \int_0^1 d\lambda \langle V_1 - V_1^{(0)} - V_0 \rangle_{\lambda}^{\rm CM}, \qquad (2.9)$$

where the superscript CM denotes a constrained average and  $V_1^{(0)}$  is the total potential energy  $V_1$  for particles located in their respective lattice positions. A linear scaling relation was conjectured, on rather general grounds, for the asymptotic behavior of the free energy as a function of the sample size:  $\beta f_{\rm ex}(N) + \ln N/N = \beta f_{\rm ex}(\infty) + \mathcal{O}(N^{-1}).^9$ 

We finally add some further considerations about the numerical implementation of the FL method. In principle, one might choose the value of c in an arbitrary way. However, if the quantity  $\Delta R^2$  for the target solid is close to  $3/(\beta c)$ , the variations of the integrand in Eq. (2.9) and, correspondingly, the error made in the numerical quadrature get very small. In practice,  $\lambda$  was taken to increase from 0 to 0.9 with steps of 0.05, and with a smaller step (0.01) in the range from 0.9 to 1. For each value of  $\lambda$ , as many as  $2\times10^4$  MC sweeps were produced at equilibrium. The MC moves were such that the position of the center of mass of the solid was held fixed; this way, particles can undergo only limited excursions along the run. For this reason, if a particle happens to move out of the simulation box, there is no need to put it back.

### **III. RESULTS**

### A. Gaussian-core model

Figure 1 presents the phase diagram of the GCM, calculated with the numerical techniques discussed above, in the temperature-pressure plane. The general features of this phase diagram have already been illustrated in a number of papers. <sup>22,23,31,32</sup> A novel feature that has been just reported is the emergence, at low densities and in a narrow range of temperatures (0.0031  $\leq T^* \leq 0.0037$ ), of a bcc phase intermediate between the fluid and the fcc phase. 18 Correspondingly, the thermodynamic coordinates of the triple point are  $T_{\rm tr}^*$ =0.0031 and  $P_{tr}^*$ =0.0070. Calculations carried out with different number of particles confirm that the reentrant bcc phase at low densities is not a finite-size effect (see the inset in Fig. 1). Tracing the coexistence lines in a phase diagram requires the calculation of the chemical potential  $\mu(T,P)$  for all candidate phases. In the case of the GCM, the reentrance of the fluid phase at high densities for  $T < T_{\text{max}}$  calls for an accurate calculation of this quantity in the dense-fluid regime. However, in such thermodynamic conditions Widom's method is no longer reliable. We thus resorted to a thermodynamic integration along a composite path in the fluidphase region: We first moved from low to high densities  $(\rho^*=0.74)$  at fixed temperature  $(T^*=0.015)$ , and followed therefrom an isochoric path down to low temperatures (T\* =0.002). Differences between the chemical potentials of fluid and solid phases were plotted as a function of the pressure in Figs. 2 and 3. The sequence of phases showing up with increasing pressures at  $T^* = 0.002$  is fluid, fcc, bcc, and fluid again. It is also apparent from Fig. 2 that the chemicalpotential gap between the fcc and bcc phases depends on the

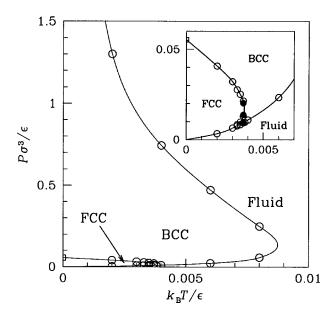


FIG. 1. Phase diagram of the GCM in the (T,P) plane: The markers (open circles) identify the states where we carried out the numerical calculations with N=1372 particles for the fluid and fcc phases and with N=1458 for the bcc phase. The triple-point region is magnified in the inset: The solid circles mark the phase thresholds in larger samples with 2048 particles for the fluid and fcc phases and with 2000 particles for the bcc phase, at  $T^*$ =0.0037. The fcc-bcc coexistence pressure at  $T^*$ =0 (open square) was taken from (Ref. 5). The lines drawn through the data points are a guide for the eye.

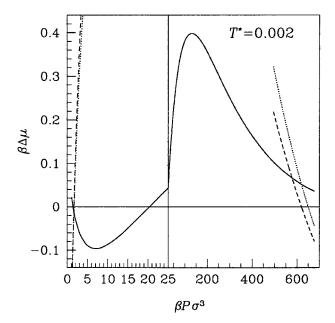


FIG. 2. Chemical-potential differences between pairs of GCM phases plotted as a function of the pressure for  $T^*$ =0.002:  $\beta\Delta\mu_{\rm fluid,fcc}$  (dashed line),  $\beta\Delta\mu_{\rm fluid,bcc}$  (dotted line), and  $\beta\Delta\mu_{\rm fcc,bcc}$  (continuous line). Upon increasing either P or  $\rho$ , the GCM exploits a fluid-fcc-bcc-fluid sequence of phases. A zoom in the low-pressure region reveals the nonmonotonic behavior of  $\beta\Delta\mu_{\rm fcc,bcc}$ , a feature that is ultimately responsible for the reentrance of the bcc phase at higher temperatures (see also Fig. 3). The lines are spline interpolants of the data.

pressure in a distinctly nonmonotonic way: At low pressures, the bcc phase already competes with the fcc phase and is about to become stable. The changeover from the fcc to the bcc phase occurs at higher temperatures. In fact, the shallow valley in the quantity  $\mu_{\rm fcc} - \mu_{\rm bcc}$  gradually slides upwards with the temperature until, for  $T^* \gtrsim 0.0030$ , the bcc phase

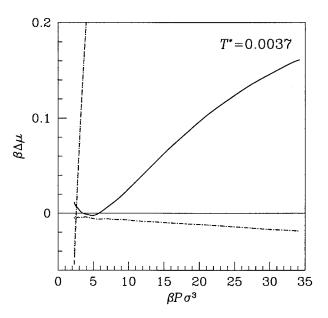


FIG. 3. Chemical-potential differences between pairs of GCM phases plotted as a function of the pressure for  $T^*$ =0.0037:  $\beta\Delta\mu_{\rm fluid,fcc}$  (dashed line),  $\beta\Delta\mu_{\rm fluid,bcc}$  (dotted line),  $\beta\Delta\mu_{\rm fluid,fcc}$  (dash-dotted line), and  $\beta\Delta\mu_{\rm fcc,bcc}$  (continuous line). The lines for  $\beta\Delta\mu_{\rm fluid,fcc}$  and  $\beta\Delta\mu_{\rm fluid,bcc}$  are hardly resolved on the scale of the figure. Upon increasing the pressure, the GCM exploits a fluid-bcc-fcc-bcc-fluid sequence of phases. The lines are spline interpolants of the data.

TABLE I. Excess Helmholtz free-energy per particle  $f_{\rm ex}$ , in units of  $k_BT$ , for some crystalline states of the GCM: fcc (N=1372), hcp (N=1440), and bcc (N=1458). For  $T^*$ =0.003 and 0.006, the tabulated values refer to systems with 864 and 1024 particles, respectively. The value of the reduced elastic constant  $c^*$ = $c\sigma^2/\epsilon$ , playing a role in the Frenkel-Ladd calculation, is also displayed in square brackets: For such values of c, the mean-square displacement of the Einstein solid approximately matches the mean-square deviation of a GCM particle from its reference lattice site.

| $ ho^*$  | $T^*$  | fcc (N=1372)   | hcp $(N=1440)$   | bcc (N=1458)   |
|--|--|--|------------------|--|
| 0.30<br>0.24<br>0.24<br>0.24<br>0.24<br>0.24<br>0.30<br>0.24 | 0.0020<br>0.0030<br>0.0033<br>0.0035<br>0.0037<br>0.0038<br>0.0040<br>0.0060 | 195.703(2) [0.30]<br>86.251(2) [0.35]<br>78.994(1) [0.34]<br>74.835(1) [0.33]<br>71.122(2) [0.33]<br>69.411(2) [0.32]<br>101.074(2) [0.29]<br>46.025(2) [0.29] | 71.141(1) [0.37] | 195.312(1) [0.45]<br>86.057(1) [0.39]<br>78.814(1) [0.38]<br>74.666(1) [0.38]<br>70.961(1) [0.38]<br>69.254(1) [0.37]<br>100.894(1) [0.42]<br>45.929(1) [0.35] |
| 0.24   | 0.0080   | 35.781(2) [0.24]   |                  | 35.710(1) [0.31]   |

slips in between the fluid and the fcc phases. As also seen from Fig. 3, the hcp phase never comes into play.

The excess Helmholtz free energies calculated for some solid phases of the GCM are given in Table I, together with the values of the reduced elastic constant  $c^* = c\sigma^2/\epsilon$ . Though one single FL calculation would be sufficient to estimate the free energy of any given phase in any other thermodynamic state, we found it more practical to repeat the calculation rather than generating a dense mesh of thermodynamic paths. As illustrated in Fig. 4, the free energy scales asymptotically with N as conjectured by Polson  $et\ al.$ 

The thermodynamic properties of the GCM at fluid-solid

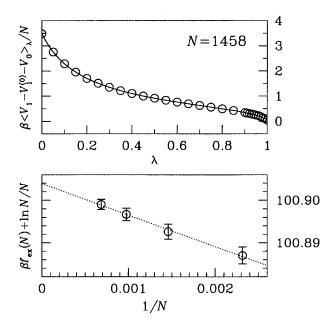


FIG. 4. Frenkel-Ladd calculation of the free energy of the GCM solid. Top: The integrand of Eq. (2.9) plotted as a function of  $\lambda$  for a bcc solid with 1458 particles ( $\rho^*$ =0.3,  $T^*$ =0.004); the continuous line is a spline interpolant of the data, the error bars being much smaller than the size of the symbols. Bottom: The quantity  $\beta f_{\rm ex}(N) + \ln N/N$  plotted as a function of  $N^{-1}$  for a bcc solid in the same thermodynamic state, with N=432, 686, 1024, and 1458. We checked the asymptotically linear scaling of the above quantity also for other states among those listed in Table I.

TABLE II. Thermodynamic properties of the GCM at fluid-solid and solid-solid coexistence. With the only exception of the states identified by  $T^*$ =0.003 and 0.006, the simulation data refer to samples with N=1372 (fluid and fcc) and N=1458 particles (bcc). For  $T^*$ =0.003 and 0.006, the tabulated values are relative to samples with 864 and 1024 particles, respectively. We show, from left to right, the values relative to the following first-order phase transitions: freezing of the fluid into either a fcc or bcc solid, bcc-to-fcc transition, fcc-to-bcc transition, and high-density melting of the bcc solid. We indicated with  $\rho_f$  and  $\rho_m$  the freezing and melting densities, respectively. All data were arbitrarily rounded off; note, however, that the error originating from the limited precision of both the Monte Carlo data *and* the free-energy values may be actually larger than that apparently implied by the chosen truncation.

| $T^*$  | $P^*/T^*$ | $\rho_f^*$ | $\rho_m^*$ | $P^*/T^*$ | $ ho_{ m bcc}^*$ | $ ho_{ m fcc}^*$ | $P^*/T^*$ | $ ho_{ m fcc}^*$ | $ ho_{ m bcc}^*$ | $P^*/T^*$ | $\rho_m^*$ | $\rho_f^*$ |
|--------|-----------|------------|------------|-----------|------------------|------------------|-----------|------------------|------------------|-----------|------------|------------|
| 0.0020 | 1.653     | 0.0779     | 0.0800     | • • •     |                  |                  | 20.360    | 0.1616           | 0.1618           | 650.20    | 0.6855     | 0.6863     |
| 0.0030 | 2.146     | 0.0918     | 0.0938     | • • •     | • • • •          | • • •            | 10.713    | 0.1494           | 0.1496           |           |            |            |
| 0.0033 | 2.324     | 0.0961     | 0.0978     | 2.520     | 0.1002           | 0.1003           | 8.397     | 0.1426           | 0.1427           |           |            |            |
| 0.0035 | 2.369     | 0.0980     | 0.0998     | 2.789     | 0.1046           | 0.1047           | 7.187     | 0.1382           | 0.1383           |           |            |            |
| 0.0037 | 2.537     | 0.1014     | 0.1031     | 3.510     | 0.1134           | 0.1135           | 5.784     | 0.1315           | 0.1316           |           |            |            |
| 0.0038 | 2.537     | 0.1020     | 0.1038     | • • •     | • • • •          | • • •            | • • •     | • • • •          | •••              |           |            |            |
| 0.0040 | 2.730     | 0.1057     | 0.1074     | • • •     | • • • •          | • • •            | • • •     | • • • •          | •••              | 185.90    | 0.5219     | 0.5230     |
| 0.0060 | 3.893     | 0.1317     | 0.1332     | • • •     | • • • •          | • • •            | • • •     | • • • •          | •••              | 78.670    | 0.4208     | 0.4220     |
| 0.0080 | 7.285     | 0.1784     | 0.1792     | •••       | •••              | •••              | •••       | •••              | •••              | 31.172    | 0.3158     | 0.3166     |

and solid-solid coexistence are given in Table II. Upon increasing the pressure for temperatures just above the triple point, the entropy per particle drops by about  $0.8k_B$  and  $0.1k_B$ across the fluid-to-bcc and bcc-to-fcc phase transitions, respectively. However, the next jump at the fcc-to-bcc transition is positive in that the entropy of the coexisting bcc phase, notwithstanding its slightly higher density (see Table II), again exceeds that of the fcc solid by about the same amount  $(0.1k_R)$ . As then implied by the Clausius-Clapeyron equation, the slope of the higher-pressure branch of the fccbcc coexistence line is negative in the (T, P) plane as is also the slope of the upper branch of the bcc-fluid coexistence line. In fact, at the reentrant melting point, the coexisting fluid has both a larger density and a larger entropy than the bcc phase, the entropy jump being again of the order of  $0.8k_B$ per particle.

We actually found that for low densities  $(\rho^* \leq 0.2)$  the entropy of the bcc solid systematically overcomes that of the fcc solid, even below the triple-point temperature. The gap decreases slowly with increasing temperatures and is likely due to the larger number of soft shear modes hosted by the bcc structure. Actually, even at low temperatures, bccordered grains are expected to form in the freezing fluid, a circumstance which may slow down the crystallization process. On the energy side, the scales tip instead in favor of the fcc solid. In fact, at low densities ( $\rho^* \leq 0.17$ ), the fcc phase has a lower energy than the bcc phase for  $T^* \leq 0.008$ . Not surprisingly, this temperature is very close to the reduced triple-point temperature predicted by Lang et al. 23 These authors actually used the Gibbs-Bogoliubov inequality to optimize a harmonic model of both solid phases. Considering the fact that the fcc-bcc transition occurs at rather low densities, the above approximation does likely underestimate the (relative) entropies of the competing crystalline phases. As a result, the fcc phase turns out to be stable in a much more extended region than that predicted by free-energy calculations carried out with the FL method (see also Fig. 2 of Ref. 18).

As shown in Fig. 1, we predict that the bcc phase is stable for temperatures lower than  $T_{\text{max}}^* \simeq 0.00874$ . The reduced density and pressure of the solid coexisting with the

fluid at this temperature are  $\rho_{\rm max}^* \approx 0.239$  and  $P_{\rm max}^* \approx 0.128$ , respectively. At this bending point the bcc solid melts, upon heating, with no volume change. However, the transition is still first order since the entropy per particle of the fluid is  $0.79k_B$  larger than in the solid. As for the fcc phase, our current estimate for the uppermost fcc-bcc coexistence temperature is 0.0038. The corresponding estimates for the reduced density and pressure attained by the system in this external state of the fcc stability basin are 0.123 and 0.0174, respectively. Comments analogous to those made above on the nature of the bcc-fluid phase transition at the maximum temperature of the coexistence line can be straightly extended to the fcc-bcc transition as well.

Figure 5 shows the RDFs of the fluid and solid phases for  $T^*$ =0.004, at both ordinary and reentrant melting densities. We note that neighboring particles lie, on average, at relative distances larger than  $\sigma/\sqrt{2}$ , which is where the Gaussian potential inflects.

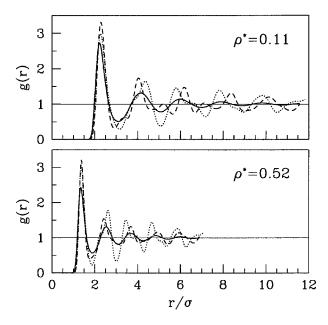


FIG. 5. Radial distribution functions of fluid and solid phases of the GCM for  $T^*$ =0.004 and  $\rho^*$ =0.11 (top) and  $\rho^*$ =0.52 (bottom): fluid (continuous line), bcc (dotted line), and fcc (dashed line).

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TABLE III. Excess Helmholtz free energy per particle  $f_{\rm ex}$ , in units of  $k_BT$ , for some crystalline states of the IPL model: fcc (N=1372), hcp (N=1440), and bcc (N=1458). The value of the reduced elastic constant  $c^* = c\sigma^2/\epsilon$  is also displayed in square brackets (see the caption of Table I).

| 1/n  | $ ho^*$ | fcc (N=1372)     | hcp (N=1440)     | bcc (N=1458)    |
|------|---------|------------------|------------------|-----------------|
| 0.10 | 2.5     | 50.350(1) [1900] |                  | •••             |
| 0.12 | 2.5     | 39.027(1) [890]  |                  | 39.397(2) [340] |
| 0.14 | 3.0     | 47.700(1) [850]  | 47.708(1) [870]  | 47.943(2) [490] |
| 0.15 | 3.5     | 59.180(1) [1010] |                  | 59.423(2) [600] |
| 0.16 | 4.0     | 69.608(1) [1100] | 69.624(1) [1110] | 69.833(2) [700] |
| 0.17 | 3.5     | 50.607(1) [570]  |                  | 50.687(2) [400] |
| 0.20 | 5.0     | 76.881(1) [690]  | 76.926(1) [680]  | 76.947(1) [540] |

# B. Inverse-power-law model

We list the excess Helmholtz free energies for some crystalline states of the IPL model in Table III. Figure 6 shows the chemical potential plotted as a function of the pressure for an intermediate value of the softness parameter 1/n=0.16. Upon increasing  $\gamma$ , the IPL fluid freezes into a bcc structure. A further compression triggers a solid-solid transition into a fcc structure. Correspondingly, the equation of state (Fig. 7) shows two tie lines joining the three distinct branches at the fluid-bcc and bcc-fcc transition points. We found that the hcp solid is systematically less stable than the fcc solid, although the chemical-potential gap between the two phases is rather small at all pressures. As n grows, the range of bcc stability gradually reduces until, for 1/n $\leq 0.14$ , the fcc structure only is left over. The maximum value of the power exponent for which the bcc solid is thermodynamically stable is close to 7 (0.14  $\leq$  1/n < 0.15). The phase diagram of the IPL fluid is shown in Fig. 8 while the phase-transition densities are listed in Table IV. In the triple-

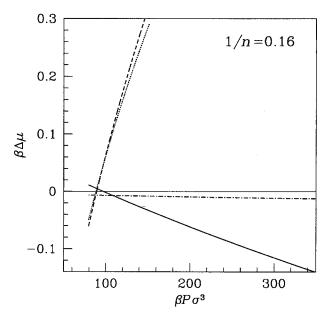


FIG. 6. Chemical-potential differences between pairs of phases of the IPL fluid for 1/n=0.16, plotted as a function of the pressure for  $T^*$ =1:  $\beta\Delta\mu_{\rm fluid,fcc}$  (dashed line),  $\beta\Delta\mu_{\rm fluid,fcc}$  (dotted line),  $\beta\Delta\mu_{\rm fcc,bcc}$  (dash-dotted line), and  $\beta\Delta\mu_{\rm fcc,bcc}$  (continuous line). For increasing pressures, the IPL fluid exploits a fluid-bcc-fcc sequence of phases. The lines are spline interpolants of the data.

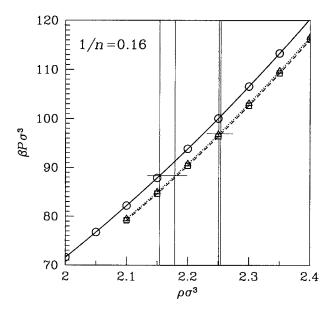


FIG. 7. Equation of state of the IPL model for  $T^*=1$  and 1/n=0.16. The fluid branch  $(\bigcirc$ , continuous line) and the fcc branch  $(\square$ , dashed line) were plotted for N=1372 particles, while the bcc branch  $(\triangle$ , dotted line) was obtained with a sample of 1458 particles. The coexistence densities, signaled by two pairs of thin vertical lines, are located where the tie lines cross different branches of the equation of state.

point region, the density jumps are approximately 0.030 across the fluid-bcc transition and 0.004 across the bcc-fcc transition; correspondingly, the entropy decreases at each transition by about  $0.7k_B$  and  $0.1k_B$  per particle, respectively. All along the freezing line, the entropy of the bcc solid overcomes that of the fcc solid by approximately  $0.1k_B$  per particle. We verified that the estimate of the power exponent  $n_{\rm tr}$  for which the IPL model exhibits triple-phase coexistence is

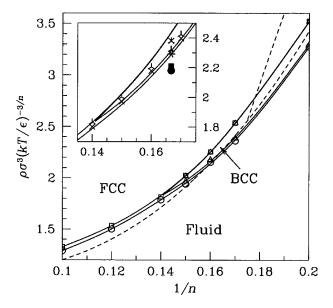


FIG. 8. Phase diagram of the IPL potential: fluid (N=1372, open circles), fcc (N=1372, open squares), and bcc (N=1458, open triangles). The continuous lines drawn through the data are a guide for the eye. The dashed lines are the phase thresholds reported in Ref. 33. In the inset, we compare the present data (continuous lines) with the phase-transition loci reported in Ref. 25 (n=6: fluid, solid circle; fcc, solid square), in Ref. 26 (n=6: fluid, star; bcc, tripod; fcc, cross), and in Ref. 27 (fluid, cross; solid, tripod; note that this latter datum refers to fcc for 1/n<0.16 and to bcc otherwise).

TABLE IV. Thermodynamic properties of the IPL model at fluid-solid and solid-solid coexistence for some values of the softness parameter 1/n. The tabulated data refer to samples with N=1372 (fluid and fcc) and N=1458 particles (bcc). All data were arbitrarily rounded off at the third decimal digit (see the caption of Table II).

| 1/n  | $P^*/T^*$ | $ ho_f^*$ | $ ho_m^*$ | $P^*/T^*$ | $ ho_{ m bcc}^*$ | $ ho_{	ext{fcc}}^*$ |
|------|-----------|-----------|-----------|-----------|------------------|---------------------|
| 0.10 | 29.747    | 1.289     | 1.327     |           | •••              |                     |
| 0.12 | 41.810    | 1.501     | 1.534     | • • •     |                  | • • • •             |
| 0.14 | 60.507    | 1.787     | 1.817     | • • •     |                  | • • • •             |
| 0.15 | 71.151    | 1.942     | 1.968     | 76.945    | 2.020            | 2.024               |
| 0.16 | 88.329    | 2.154     | 2.179     | 96.950    | 2.251            | 2.254               |
| 0.17 | 105.614   | 2.362     | 2.387     | 124.717   | 2.534            | 2.537               |
| 0.20 | 203.334   | 3.274     | 3.297     | 240.225   | 3.518            | 3.521               |

not affected by appreciable finite-size effects because of the large samples used, the only significant source of error being the limited statistics of the simulation. The maximum error expected on  $\beta\Delta\mu$ , near to freezing, is approximately equal to  $1.5\times10^{-2}$ , as for the GCM. Such an error would, in turn, affect the estimates of the reduced phase-transition densities by an amount not greater than  $3\times10^{-2}$ . We conclude that the error on  $n_{\rm tr}$  should not be larger than 0.5.

Figure 8 presents the phase diagram of the IPL model, spanned by the softness parameter 1/n and by the scaled quantity  $\gamma$ . We also plotted fluid-solid coexistence data obtained by other authors using different approaches. <sup>25–27,33</sup> The data reported in Ref. 25 refer to a single-occupancy solid in which each particle is confined within a spherical cell whose diameter is set equal to the fcc nearest-neighbor lattice spacing. Dubin and Dewitt estimated the fluid-solid and solid-solid coexistence of the IPL model by applying the empirical Lindemann criterion, including some anharmonic contributions to the internal energy of the solids. <sup>34</sup> Their fluid-fcc coexistence line almost coincides with the present fluid-solid coexistence line; instead, the location of the bcc threshold does not agree with the present data.

### **IV. DISCUSSION**

The low-density/low-temperature topology of the phase diagram of the GCM, with a triple point separating a region where the fluid freezes into a fcc structure from another region where such two phases are bridged by an intermediate bcc phase, is common to other model systems with softly repulsive interactions. Another example, besides the GCM and the IPL model, is the Yukawa potential  $v_{y}(r)$  $=B \exp(-r/\ell)/r$  (with B > 0), which has been used to model the thermal behavior of dilute solutions of charged colloids with counterions. 11-13 The phase diagram of this latter model can be conveniently spanned by two scaled quantities, i.e.,  $\rho \ell^3$  and  $B \rho^{1/3} / (k_B T)^{1/2}$ . In an attempt to relate the phase behaviors of the Gaussian and Yukawa potentials to that of the IPL model, we required in Ref. 18 the logarithmic derivatives of the three potentials to match, at least for separations close to the average nearest-neighbor distance  $\bar{r} = \rho^{-1/3}$ . This condition yields two "optimal" values for the IPL power exponent:  $n_G = 2(\rho\sigma^3)^{-2/3}$  and  $n_Y = 1 + (\rho\ell^3)^{-1/3}$ , respectively. Increasing the density of the Gaussian and Yukawa models along the freezing line is tantamount, through the above relations, to an increase of the softness parameter 1/n of the "equivalent" IPL model. In both cases the system is driven towards the bcc phase. The values of  $n_G$  and  $n_Y$  calculated at the triple point of the Gaussian and Yukawa potentials are 9.6 and 12.0, respectively, not too far from the IPL value ( $\approx$ 7). This rough argument shows that it is possible to gauge the softness of such potentials in such a way that their phase behavior is referred to a common frame where the bcc phase is ultimately promoted by a sufficiently soft interaction.

A similar interplay between bcc and fcc solid phases is also present in the phase diagram of the modified Buckingham potential that is used to model the behavior of rare gases at high temperature and pressure:<sup>35</sup> Under extreme thermodynamic conditions close to freezing, notwithstanding the presence of an attractive tail, particles feel almost exclusively the repulsive shoulder of the potential, whose softness increases with the temperature.

### **V. CONCLUSIONS**

In this paper we revisited the phase diagram of two classical reference models for the liquid state, both governed by softly repulsive interactions with Gaussian and inversepower-law shapes, respectively. The aim of this effort was to point out some aspects of the phase diagrams which had been previously overlooked or simply ignored, in a common theoretical framework for repulsive pair potentials that decrease polynomially or faster with the interparticle distance. To this end, we carried out extensive Monte Carlo simulations and calculated the thermodynamic properties of both fluid and solid phases through the combined use of thermodynamic integration techniques and free-energy calculations. We further discussed the similarities and semiquantitative correspondences in the phase diagrams of such models in relation to the softness of the potential and with specific reference to the interplay of fluid, bcc, and fcc crystalline phases.

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